# Simulations of jet - environment interactions using the PLUTO code

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Jet - environment interactions can produce interesting astrophysical phenomena that may explain features in jets such as the HST-1 in M87. Using the PLUTO code (v4.0) by A. Mignone et al., we simulate the interaction between a relativistic, magnetized, axisymmetric jet with a selection of different environments, assuming that the poloidal component of the magnetic field is negligible in large distances from the source. Two different simulations are presented: the jet interacts with either a static atmosphere (first case) or with accreting material (second case). These interactions are explored by performing magnetohydrodynamic simulations of both the jet and the static atmosphere or the Bondiaccretion. A transition in the shape of the jet from parabolic to conical near the Bondi radius was observed by Asada & Nakamura in the case of M87, which may be connected to pressure variations of the accreting material outside the jet. Consequently, the second case aims to examine whether such pressure variations may be produced by Bondi accretion and thus change the shape of the jet.

Subject :	:	oral
Topics	:	Plasmaphysics
Topics	:	Astrophysics
Topics	:	Numerical simulations

Accretion and Outflows throughout the scales, 1-3 October, Lyon, France

# Simulations of jet - environment interactions using the PLUTO code

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# Aknowledgements

- Collaborators: N. Vlahakis & G. Katsoulakos K. Sapountzis
- T. Matsakos
- State Scholarship Foundation

# Outline



 $\bullet$  A glimpse of M87

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## 1 Introduction

• A glimpse of M87

## 2 Simulations

- Integrals
- Acceleration
- Jet & Bondi Accretion
- Jet & Static Atmosphere
- Rarefaction

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## 1 Introduction

• A glimpse of M87

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## **3** Conclusions & Future work

A glimpse of M87



M87 at 90cm, (Owen et al. 2000)

A glimpse of M87

# Some values...

- One of the AGNs closest to Earth (16.7 Mpc)
- Mass: 3.2 to 6.6  $\cdot 10^9 M_{\odot}$

A glimpse of M87

# Some values...

- One of the AGNs closest to Earth (16.7 Mpc)
- Mass: 3.2 to 6.6  $\cdot 10^9 M_{\odot} \rightarrow 1 mas = 0.081 pc = 140 R_S$
- Viewing angle of inner jet regions:  $10^o 19^o$  to the line of sight
- HST-1: Luminous region at  $\sim 0.9$  arcsec from core

A glimpse of M87



Core of the M87 jet with frequency (Hada et al. 2011)

A glimpse of M87



Jet radius with deprojected distance from core (in Schwarzschild radii, Asada & Nakamura, 2012)

A glimpse of M87

A glimpse of M87

# A possible explanation ?

• The HST-1 complex is located at  $\simeq 5 \cdot 10^5 R_S$  from the core

A glimpse of M87

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A glimpse of M87

- The HST-1 complex is located at  $\simeq 5 \cdot 10^5 R_S$  from the core
- This distance corresponds to the Bondi radius
- Is it possible that accreting material can cause the observed change in the shape of the jet ?
- Simulations of both the jet and the Bondi accretion

A glimpse of M87



Integrals Acceleration Jet & Bondi Accretion Jet & Static Atmosphere Rarefaction

# Setting up the jet

- Initial Lorentz factor:  $\gamma=5$
- Maximum magnetization:  $\sigma = 4$
- Density: defined by  $\sigma = \frac{B^2}{\gamma^2 \rho} \Big|_{\theta = \theta_1}$
- Thermal pressure: polytropic with  $\Gamma = 5/3, c_s = 0.1$

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Integrals Acceleration Jet & Bondi Accretion Jet & Static Atmosphere Rarefaction

# Modifying the integrals

Assuming axisymmetry and time independence, we may partially integrate the ideal MHD equations:

• Mass flux to magnetic field flux ratio:

$$\Psi_A = \Psi(A) = \frac{4\pi\gamma\rho_o V_p}{B_p}$$

• Field angular velocity:

$$\Omega = \Omega(A) = \frac{V_{\phi}}{\varpi} - \frac{V_p}{\varpi} \frac{B_{\phi}}{B_p}$$

• Total specific angular momentum:

$$L = L(A) = \xi \gamma \varpi V_{\phi} - \frac{\varpi B_{\phi}}{\Psi_A}$$

#### Integrals

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• Total energy to mass flux ratio:

$$\mu = \mu(A) = \xi \gamma - \frac{\varpi \Omega B_{\phi}}{\Psi_A c^2}$$

• Adiabat:

$$Q = Q(A) = \frac{P}{\rho_o^{\Gamma}}$$

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Assuming no poloidal component is used, the integrals may be expressed as:

• Specific angular momentum:

$$L = \xi \gamma r sin(\theta) V_{\phi} = \xi \gamma \varpi V_{\phi}$$

• Angular velocity function:

$$\Phi = -\frac{B_{\phi}}{4\pi\gamma\rho_o crsin(\theta)} = -\frac{B_{\phi}}{4\pi\gamma\rho_o c\varpi}$$

• Total energy to mass flux ratio:

$$\mu = \xi \gamma + \frac{B_{\phi}^2}{4\pi \gamma \rho_o c^2}$$

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# Acceleration

Using the integrals:

Wind equation (velocity along a field line):

$$\frac{\mu^2}{\xi^2} \frac{G^2 \left(1 - M^2 - x_A^2\right)^2 - x_A^2 \left(G^2 - M^2 - x^2\right)}{G^2 \left(1 - M^2 - x^2\right)} = 1 + \left[\frac{\sigma_M M^2 \varpi \vec{\nabla} A}{\xi x^2 A}\right]^2$$

x cylindrical radius (normalized to the light cylinder),  $x_A$  its value on Alfvén surface,  $G=x/\!x_A,\,\sigma_M=A\Omega^2/\Psi_Ac^3$ 

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### **Transfield equation** (shape of a field line):

$$\begin{split} \left[x^2 \left(\vec{\nabla}A\right)^2 & \frac{\mathrm{d}ln(\frac{x_A}{\varpi_A})}{\mathrm{d}A} - \bar{L}A \left(1 - M^2 - x^2\right)\right] \left(\frac{\vec{\nabla}A}{\varpi}\right) \\ &+ \left[\frac{2x_A^2}{\varpi_A^3 G} \left(\vec{\nabla}A\right)^2 + \frac{\mu^2 x_A^6 A^2}{\varpi_A^5 \sigma_M^2 M^2 G^3} \left(\frac{G^2 - M^2 - x^2}{1 - M^2 - x^2}\right)^2\right] \hat{\varpi} \cdot \vec{\nabla}A \\ &- \frac{M^2}{2} \vec{\nabla} \left[ \left(\frac{\vec{\nabla}A}{\varpi}\right)^2\right] \cdot \vec{\nabla}A - \frac{\Gamma - 1}{\Gamma} \vec{\nabla} \left[\frac{\xi(\xi - 1)}{M^2} \frac{A^2 x_A^4}{\sigma_M^2 \varpi_A^4}\right] \cdot \vec{\nabla}A \\ &- \frac{1}{2\varpi^2} \vec{\nabla} \left[ \frac{\mu^2 A^2 x_A^6}{\sigma_M^2 \varpi_A^2} \left(\frac{1 - G^2}{1 - M^2 - x^2}\right)^2\right] \cdot \vec{\nabla}A = 0 \end{split}$$

- Steady state MHD equations after partial integration: wind & transfield
- Solutions depend on Alfvénic Mach number and magnetic flux function
- Wind equation solutions depend on the bunching function  $S=\varpi|\nabla A|/A=\varpi^2 B_p/A$

$$\mu^2 \frac{G^2 (1 - M^2 - x_A^2)^2 - x_A^2 (G^2 - M^2 - x^2)}{G^2 (1 - M^2 - x^2)^2} = 1 + \left(\frac{\sigma_M M^2 \varpi \nabla A}{x^2 A}\right)^2$$

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#### Desirable form of S?

• Using the integrals:

$$\frac{d\gamma}{dx} = \gamma^2 \sigma_M (\gamma^2 - 1)^{1/2} \frac{dS/dx}{\mu - \gamma^3}$$

For an accelerated flow:

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# Important results

In each simulation we examine:

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- Bunching function...

N.Vlahakis & A. Königl 2003, C.Fendt & R.Ouyed 2004, D. Millas et. al 2014, S. S. Komissarov et al. 2009

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- Solvability condition...
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- Solvability condition...
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- ...and of course the shape of the jet

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# Jet - Bondi accretion

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# Jet - Bondi accretion

• Grid:  $r: 10^4 - 10^5$ ,  $\theta: 0.001 - \pi/2$ 

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- Grid:  $r: 10^4 10^5$ ,  $\theta: 0.001 \pi/2$
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  - $r = 10^4$ : userdef
  - $r = 10^{5}$ :
  - $\theta = 0.001$ : axisymmetric
  - $\theta = \pi/2$ : eqtsymmetric
Integrals Acceleration Jet & Bondi Accretion Jet & Static Atmosphere Rarefaction

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Proper speed at 0, 1, 10 and 20 sound crossing times



Lorentz factor with  $\theta$  in 0, 1, 10 and 20 sound crossing times  $(r \sim 3 \cdot 10^4)$ 

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Jet - environment simulations

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L integral in 0, 1, 10 and 20 sound crossing times

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 $\Phi$  integral in 0, 1, 10 and 20 sound crossing times

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 $\mu$  integral in 0, 1, 10 and 20 sound crossing times

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# Acceleration efficiency

- Theoretical maximum of  $\gamma$ :  $\gamma_{max} = \gamma(\sigma + 1) = 25$
- Result:  $\gamma_f = 15$
- Acceleration efficiency  $\alpha \simeq 60\%$

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Solvability 
$$\left(\frac{\varpi B_{\phi}}{\gamma}\right)$$

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#### Simulation Results

• No steady state after 20 crossing times

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- Probable rarefaction acceleration

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# Problems

#### • The very existence of environment

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- Contrast of densities  $\simeq 10^5$

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- Contrast of densities  $\simeq 10^5$
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- Magnetic field diffusion

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#### Why use a static atmosphere?

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#### Why use a static atmosphere?

• Easy to analyse: 
$$\frac{dP}{dr} = -\rho \frac{GM}{r} \rightarrow \rho = \left[\rho_i^{\Gamma-1} + GM \cdot \frac{\Gamma-1}{q_o \Gamma} \cdot \left(\frac{1}{r} - \frac{1}{r_{in}}\right)\right]^{\frac{1}{\Gamma-1}}$$

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- No inequality for the upper boundary
- Outflow conditions may be used for  $r = 10^5$

But: No shock to provide the necessary pressure gradient

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Proper speed 0, 1, 2.5 10 sound crossing times





Lorentz factor to  $\theta$  for 0, 1, 2.5 and 10 sound crossing times  $(3 \cdot 10^4)$ 

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Jet - environment simulations



L integral at 0, 1, 2.5 and 10 sound crossing times

 Outline
 Integrals

 Introduction
 Acceleration

 Simulations
 Jet & Bondi Accretion

 Conclusions & Future work
 Rarefaction





 $\Phi$  integral at 0, 1, 2.5 and 10 sound crossing times





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# Acceleration efficiency

- Theoretical maximum of  $\gamma$ :  $\gamma_{max} = \gamma(\sigma + 1) = 25$
- Results:  $\gamma$ :  $\gamma_f = 14$
- Acceleration efficiency  $\alpha \simeq 56\%$
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## Simulation Results

• Steady state after 10 crossing times

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- Much more comprehensive results concerning the shape no change in steady state!

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Integrals Acceleration Jet & Bondi Accretion Jet & Static Atmosphere Rarefaction

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- Much more comprehensive results concerning the shape no change in steady state!
- Jet interior in agreement with other simulations & theory
- Probable rarefaction acceleration even with different environment!

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- Examine environment with  $\rho_{env} = \frac{\rho_j}{10}$
- Neglect gravity (GM=0)
- Mantain the same configuration for the jet



Density with  $\theta$  in 0, 1, 5 and 8 light crossing times  $(r \simeq 3 \cdot 10^4)$ 



Lorentz factor to  $\theta$  in 0, 1, 5 and 8 light crossing times  $(r \simeq 3 \cdot 10^4)$ 

## Our Goal:

An accreting environment with a pressure gradient, which would result in changing the shape of the jet

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- Jet environment interaction clearly affects the shape of the jet
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- The Bondi accretion scenario is unclear (interacting region, boundary conditions)
- In both cases, the inner jet does not change
- All other results (acceleration, shape) consistent with other simulations and theoretical work
- Both scenarios indicate a probable rarefaction acceleration in the interacting region

## Future work

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### • Use alternative initial conditons

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- Use alternative initial conditons
- Alternative way to control the boundary conditions at  $r = r_{max}$
- Reduce B-field diffusion

## Future work

- Use alternative initial conditons
- Alternative way to control the boundary conditions at  $r = r_{max}$
- Reduce B-field diffusion
- Better insight of the interacting region